

Theory of extraction

Extraction: *solving* a predefined (valuable or undesired) components *selectively* from a solid, liquid or gas mixture by the means of a solvent
 The extraction will not directly yield pure components, the solvent must be regenerated

Main tasks during extraction:



- intense contact and mixing of the raw mixture and the solvent
- sufficient contact time in order to allow the material transport of the desired component between the phases
- separation of the two phases produced during extraction (raffinate and extract)



Extraction types in a refinery

liquid – liquid extraction: aromatic extraction

supercritical extraction: aspaltene extraction

gas – liquid extraction: sour gas/fuel gas desulphurisation



Hydrogen-sulphide removal from refinery gases



Sources of light gases

- Low H₂S content fuel gas
 - Crude oil primary distillation
 - Originally present in the crude oil
 - LPG fractionation
 - Reforming

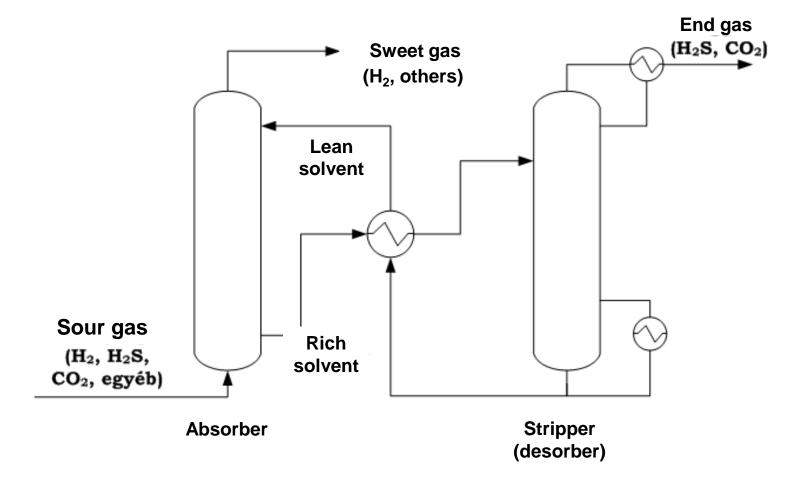
. . .

- High H₂S content H₂ rich gases
 - Hydrotreaters blowdown gas
 - FCC sour gas





Hydrogen-sulphide removal from high hydrogen concentration gases





The reaction (MDEA)

$(HO-CH_2-CH_2)_2-N-CH_3+H_2S$ \downarrow \downarrow $((HO-CH_2-CH_2)_2-NH-CH_3)^+(SH)^-$



Most frequently used absorbents

Absorbent	MEA	DEA	MDEA
Molecular weight	61	105	119
Concentration (vol%)	15	30	50
Minimum H ₂ S load (n _{H2S} /n _{amine})	0,05	0,02	0,01
Maximum H ₂ S load (n _{H2S} /n _{amine})	0,6	0,6	0,5
Capacity (H ₂ S/dm ³)	1,77	2,18	2,77

- MEA: mono-ethanol-amine
- DEA: di-ethanol-amine
- MDEA: methyl-di-ethanol-amine



Liquid – liquid extraction

The components of the raw mixture are separated by contacting the mixture with a non miscible solvent

The method of extraction

- liquid transfer from one liquid phase to the other one
- the end of the process: dynamic equilibrium (concentration)
- driving force: concentration difference between the actual vs. equilibrium concentration
- process steps: mixing, settling, separation



Liquid – liquid extraction

L-L extraction: potential applications

- L-L extraction is more economic than the distillation, if the liquid mixture boiling range is high and the valuable component is present at low concentrations.
- If the boiling point difference of the liquid components to be separated is small
- Further separation of the azeotrope mixture, formed during distillation or rectification
- If the component to be separated is sensitive to heat, or it disintegrate at higher temperatures

Requirement towards the solvent

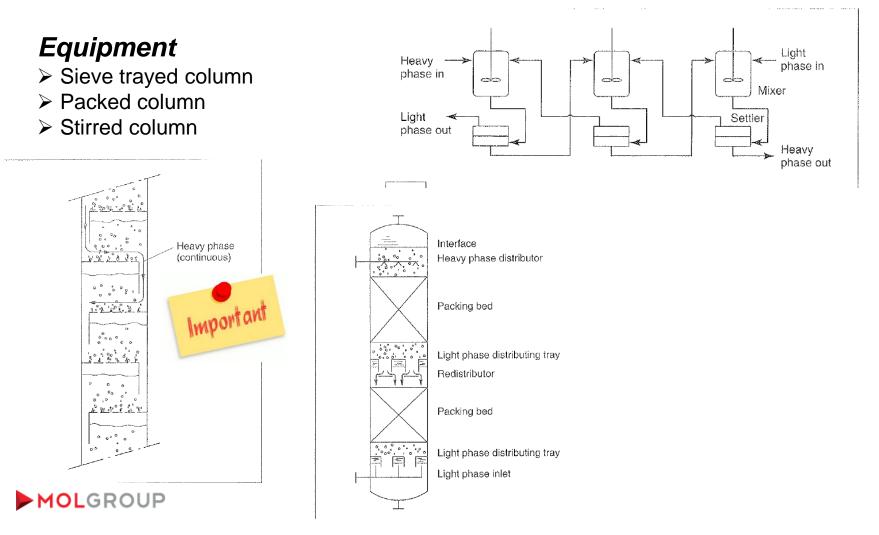
- To be selective
- To have low volatility
- ➤ To be cheap and regenerable
- Not to be solved in the liquid mixture
- Not to be corrosive nor toxic



Liquid – liquid extraction

Layout

- batch: mixing and separation in the same device
- > continuous: raw mixture input at one side, solvent on the other

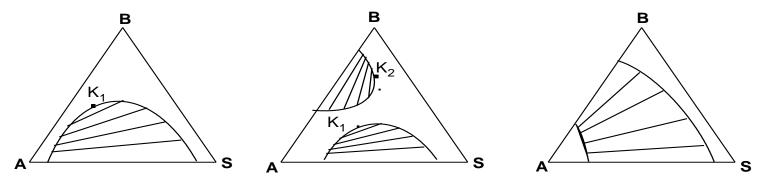


Liquid – liquid extraction equilibrium



If you mix two different liquid at under given temperature and pressure

- they may mix perfectly,
- they may limitedly mix
- > they do not mix and will form two separate phases



One critical mixing point

Two critical mixing points

No critical mixing point

- Limited mixing territory area bleow the curve (heterogeneous phase)
- Unlimited mixing territory area above curve (homogeneous phase)
- Binodes straight lines interconnecting compositions of two phases in equilibrium
- ➤ K critical mixing points

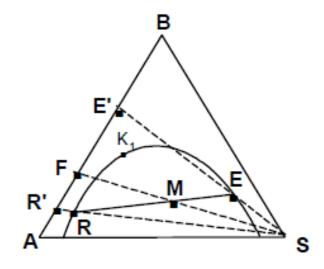


One step L–L extraction



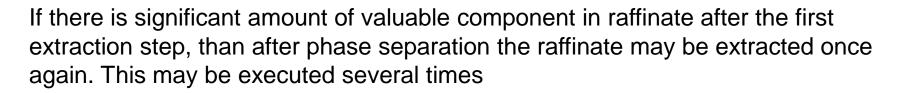
A, B are unlimitedly intermixing two liquids. After adding *S* solvent (S is mixing with A limitedly) the next diagram is produced. If you know F composition (of A and B), quantity of S and the binode, the composition of M (actual working point) can be received. If the quantity of S is adequate, than two phases will be formed: E extract and R raffinate.

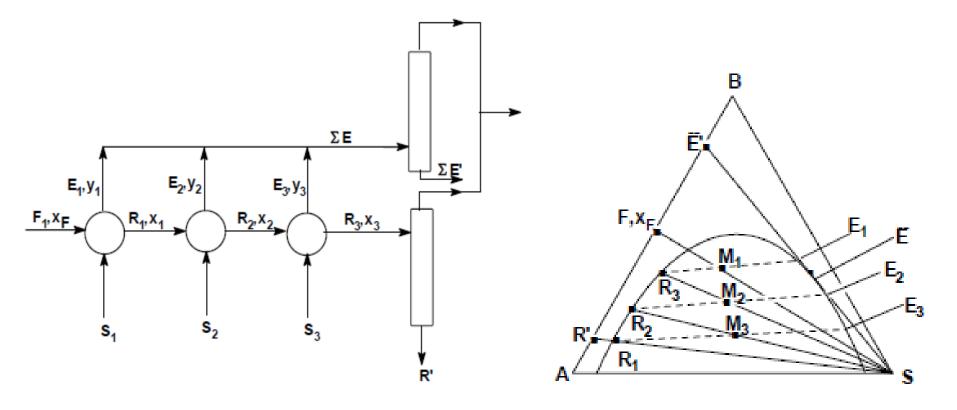
After separating the two phases and removing the solvent from extract and raffinate, $E' \stackrel{\bullet}{es} R'$ composition phases will be present.





Multi step L–L extraction with fresh solvent in U every step







Industrial utilisation of extraction

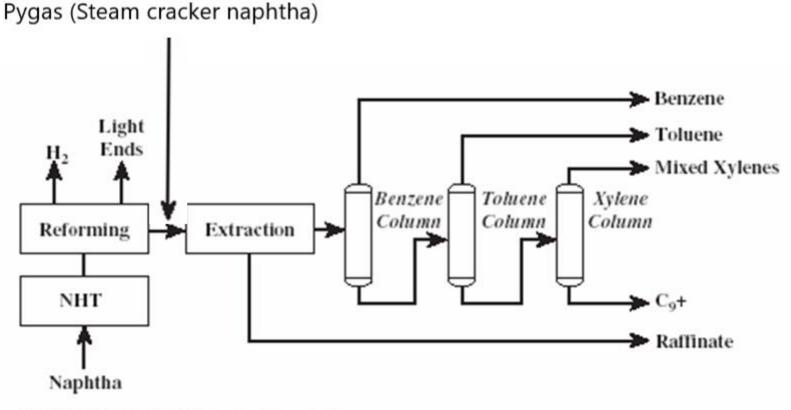
- Pigment removal from plants
- Active agent removal from herbs
- analitics: grease-oil investigation
- Pharmaceutical industry
- Oil industry aromatics extraction with TEG (tetra-ethylene-glycol)
 - asphaltene removal from vacuum residue with propane (SDA = Solvent DeAsphalting)
 - distillate extraction with NMP (N-methyl-pyrrolidone)



Aromatic production



Simple aromatic production scheme



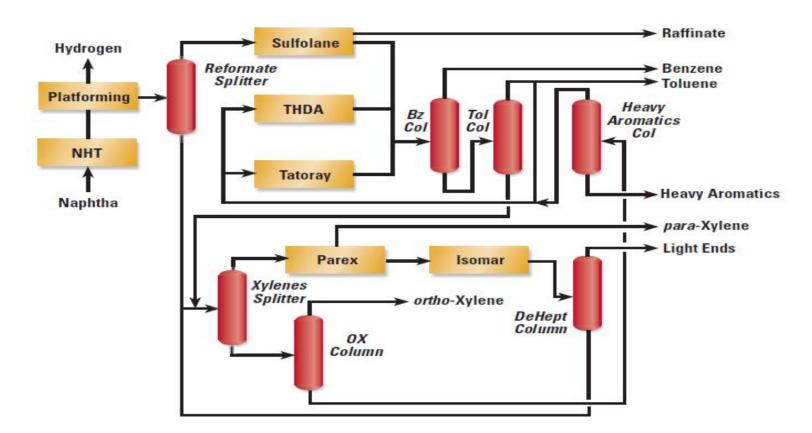
Important





Integrated aromatic production scheme – UOP

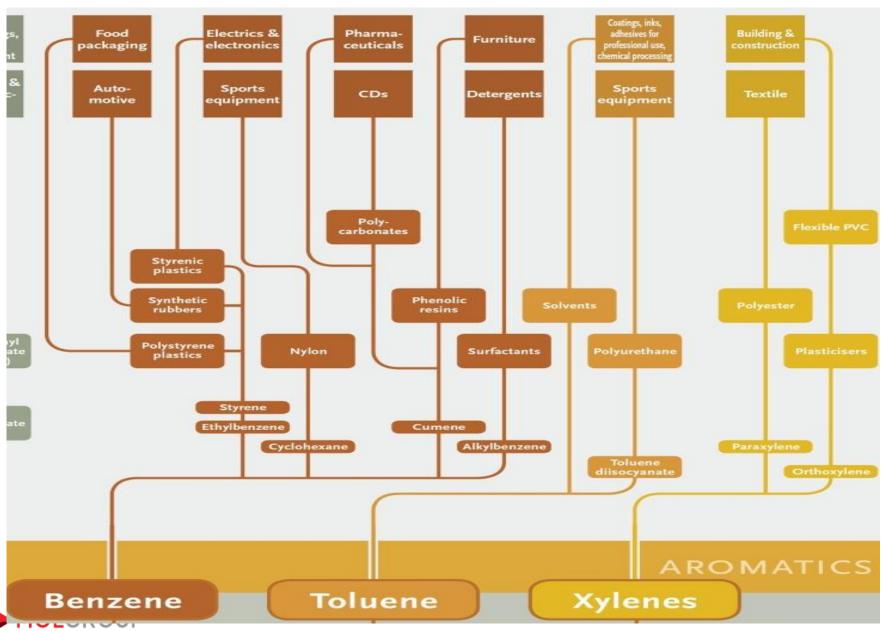




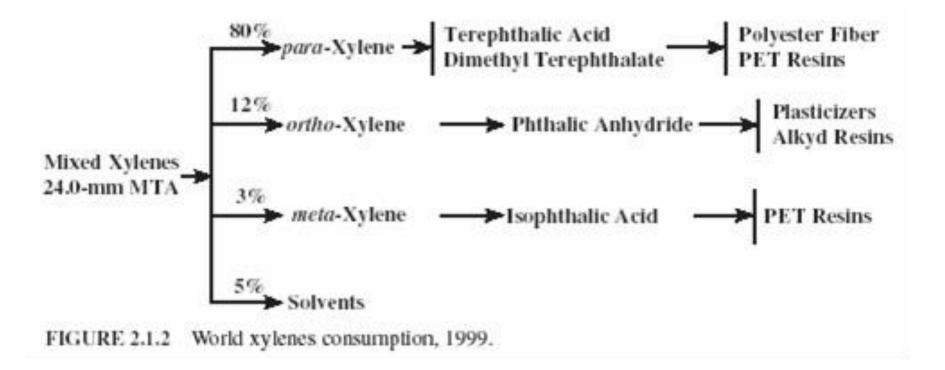
Sulfolane[™] Process – removes benzene and toluene from reformate via extractive distillation THDA[™] Process – thermal hydro-dealkylation of toluene and heavier aromatics to benzene Tatoray[™] Process – toluene and C9/C10 aromatics trans-alkylation to benzene and xylenes Parex[™] Process – high purity para-xylene removal from C8 aromatic mixture Isomar[™] Process – equilibrium composition xylene mixture production

MOLGROUP

Usage of individual aromatic components



Further usage of xylene mixtures





Requirements of the extracting solvent

High selectivity

- Thermal stability
- Chemical stability
- Low toxicity
- Low corrosivity
- Good availability
- Moderate cost
- Low enough crystallisation temperature
- Boiling point well above o-xylene boiling point (Tbp ≈ 140 °C)
- Specific gravity at least 1.1
- Viscosity at operating temperature lower than 2,5 mPas
- Solvent chemical structure
 - Small hydrocarbon ring and a polar group (this allow to solve in water and selectively in aromatics)



Aromatic extraction solvents



Pure solvent	Developed formula	M (kg/kmol)	<i>Т</i> _f (°С)	7 _b (760 mmHg) (°С)	ρ (kg/m ³) (at 20°C)	μ (mPa.s) θ (°C)
Diethyleneglycol (DEG)	Н(ОСН ₂ —СН ₂) ₂ ОН	106.1	8	245	1 116	35.7/20 0.97/140
Triethyleneglycol (TEG)	Н(ОСН ₂ —СН ₂) ₃ ОН	150.2	-7	288	1 123	49/20 0.70/140
Tetraethylene- glycol (TETRA)	Н(ОСН ₂ —СН ₂) ₄ ОН	194.2	-4	291 (300 mmHg)	1 125	61.9/20 1.8/150
Sulfolane	$H_{2}C - CH_{2}$ $ $ $H_{2}C - CH_{2}$ $G = 0$	120.2	27.6	287	1 266 (at 30°C)	10.3/30 2.5/100
N-methylpyrro- lidone (NMP)	$\begin{array}{c c} H_2C &CH_2 \\ & \\ H_2C & C=0 \\ N \\ \\ CH_3 \end{array}$	99.1	-24.4	202	1 027	1.65/25 1.3/30
N-formylmorpho- line (NFM)	$H_{2}C \qquad CH_{2}$ $ \qquad $ $H_{2}C \qquad CH_{2}$ $ \qquad $ $H_{2}C \qquad CH_{2}$ $ \qquad $ $H_{2}C \qquad CH_{2}$	115.1	20	244	1 150	8.13/20 0.65/150
Dimethylsulfo- xide (DMSO)	CH ₃ —S—CH ₃ O	78.1	18.5	189	1 080	1.99/25 1.6/35

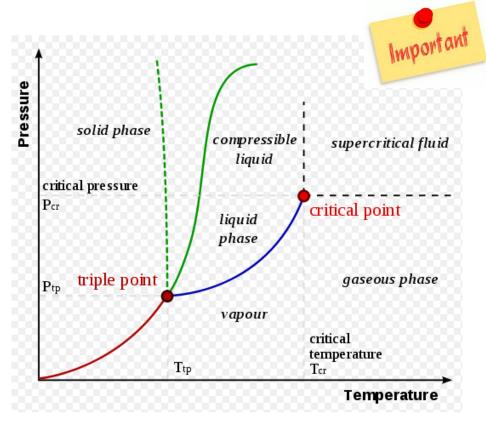


Supercritical extraction



Supercritical extraction

The valuable component is dissolved from solid or liquid raw material by the means of solvent, being in supercritical state. The extracted material is separated from the solvent by depressurization (or by adsorption, absorption.



The pressure, to be applied at critical temperature in order to make occur liquefaction, is called critical pressure.

If the material, heated above its critical temperature, is pressed with higher than its critical pressure, the material will stay homogeneous, supercritical fluid state will come into existence. The exceptionally big advantage of this close-to-supercritical-point state is that small alteration regarding the pressure will cause great alteration in specific gravity. Since the sp. gravity has a great effect on the solubility of the fluid, varying the pressure you may alter the solubility of the solvent in a wide range.

Applications of supercritical extraction

Food industry applications

- caffeine extraction from green coffee bean
- nicotine removal from tobacco
- spices extract (e.g. cinnamon, ginger, vanilla)
- > active ingredient removal from herbs (e.g. chamomile)

Environmental applications

- > purification of polluted soil (e.g. polycyclic aromatic hydrocarbons, polychlorinated biphenyls, chlor-phenols, dioxins and oil pollution)
- removal of traces of insecticide from plants

> Oil industry applications

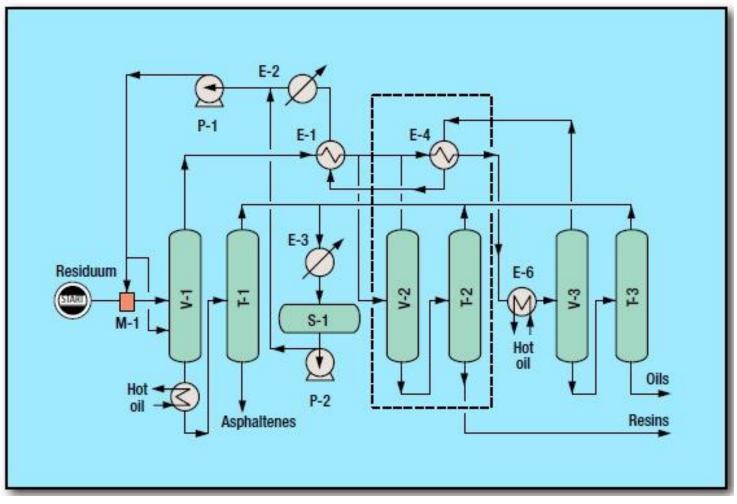
Vacuum residue extraction with C3/C4/C5 solvents

> Advantages:

- No Fired heaters
- No Compressor
- High degree of heat integration



ROSE deasphalting process by KBR



ROSE = Residuum Oil Supercritical Extraction



ROSE deasphalting process by KBR

➤ Resid is charged through a mixer (M-1), where it is mixed with solvent before entering the asphaltene separator (V-1), which uses special ROSEMAXTM internals to achieve maximum benefit of counter current solvent flow. The solvent extracts primarily non-asphaltenic, paraffinic deasphalted oil (DAO).

➤The asphaltene-rich stream leaves from the bottom of the separator and after being further heated enters the asphaltene stripper (T-1). The extracted oils and solvent flow overhead (V-1) through heat exchangers (E-1, E-4, E-6) so that the solvent reaches conditions where it exists as a supercritical fluid in which the oil is virtually insoluble.

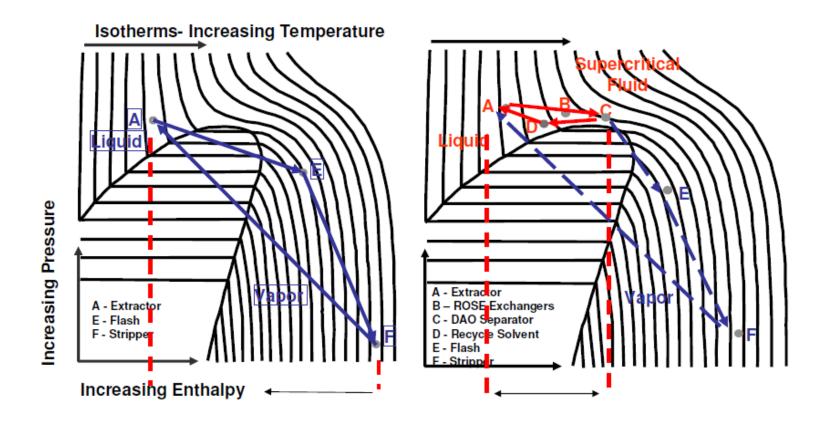
>Recovered solvent leaves the DAO separator top (V-3) to be cooled by heat exchanger (E-4, E-1) and a cooler (E-2). The only solvent vaporized is a small amount dissolved in fractions withdrawn in the separators. This solvent is recovered in the DAO product stripper (T-3). The DAO is leveas from the bottom of the DAO stripper.

>Alternately an intermediate resin rich product can be produced in V2 and T2.

Solvents range from propane through hexane and almost always are streams produced in refineries.



Conventional vs. supercritical SDA Comparison of energy demand



Conventional SDA: high energy demand

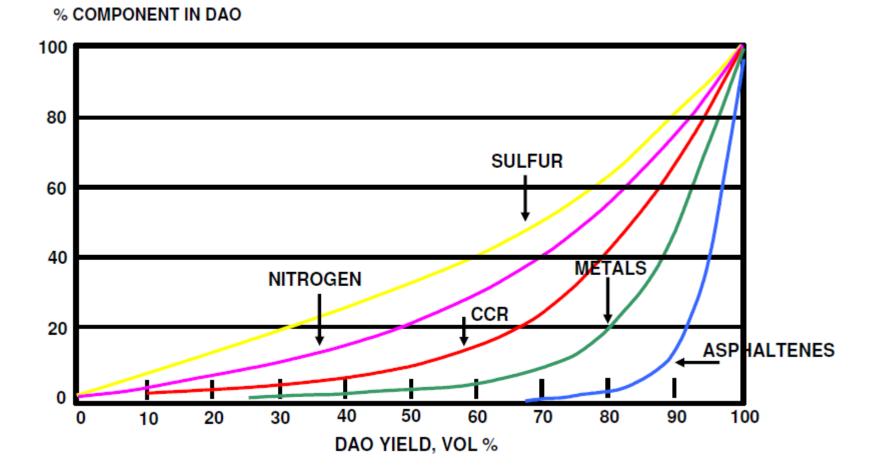
Supercritical SDA: lower energy demand



SDA = solvent deasphalting

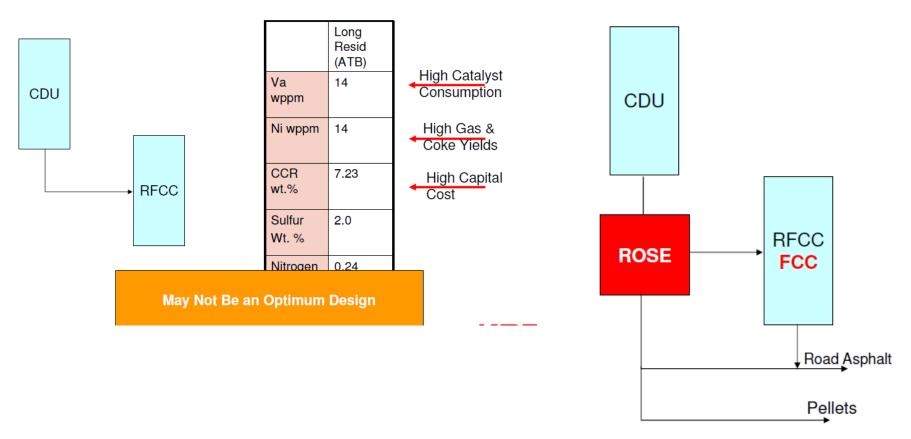


DAO product quality vs. yield



MOLGROUP

SDA applications (RFCC unit)



Gain:

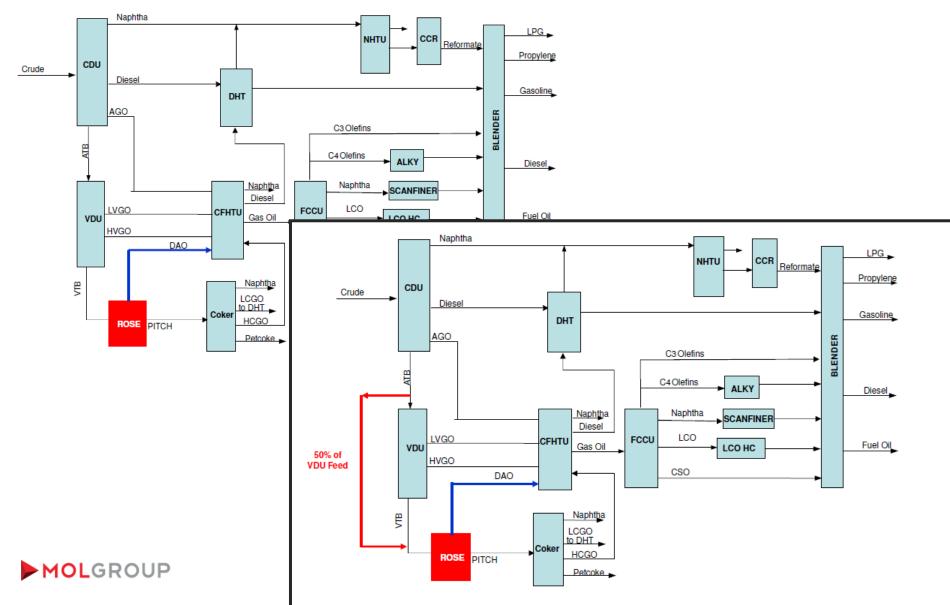
RFCC/FCC: lower catalyst cost, lower CAPEX, better conversion

> High quality road bitumen from the asphaltene (not verified in wide scale)

Peletized asphaltene (cement production, IGCC, other industrial usage)

MOLGROUP

Debottlenecking in case of heavier crude oil/capacity improvement



Important



Debottlenecking in case of heavier crude oil/capacity improvement

	Base	ROSE	VDU Bypass	Fill up Units
Crude °API	31.1	31.1	31.1	31.1
MBPSD	202	202	202	303
VDU	100	100	50	100
Coker	38	18	18	27
Coke T/D	2050	1420	1420	2130
ROSE	-	38	69	89
FCC	72	90	90	135

Message: if you introduce a SDA unit to the right point of your refinery flowscheme, you may debottleneck your old vacuum unit (VDU) and/or your delayed coker. Doing so, you may increase your overall crude processing capacity significantly, which may increase your profit.

MOLGROUP

Azeotrope and extractive distillation



Azeotrope and extractive distillation

If the relative volatility difference of the key components is low, then the energy demand of distillation is high (and the operating cost too). In this case you may add a solvent to the mixture, which has great difference in solubility towards one of the key components. The goal is to increase the relative volatility artificially. This method may be utilised during azeotrope and extractive distillation.

It is required, that the bonding of solvent and extracted material shall be not great, since in this case the cost of regeneration may be higher than the original distillation cost.

Solvent inlet possibilities

To the rectification zone: if the extracted component is removed at the bottom

> To the stripping zone: if the extracted component is removed at the top

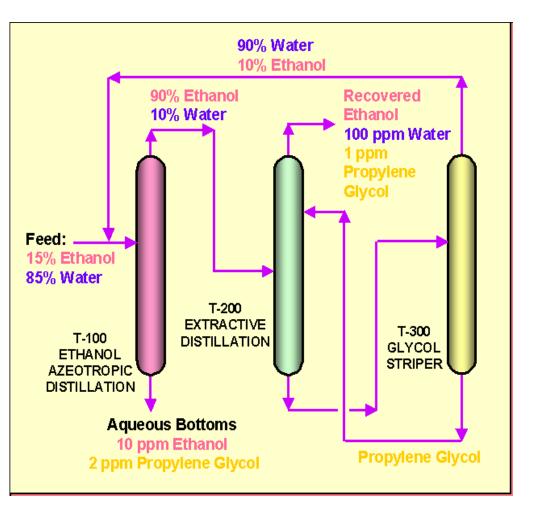


Water-ethanol separation by extractive distillation

The water-ethanol mixture forms minimum boiling point azeotrope (89,4 mol%, 96 wt% ethanol), which may be separated by propylene-glycol addition.

The first column is an azeotrope distillation. The top product is close to azeotropic concentration, the bottom is ~pure water. The upper part of the second column is rectification part, where the remaining azeotropic water is separated from ethanol. The water molecules will form bondage with the added propylene-glycol, thus increasing the relative volatility of the ethanol molecules. The top product is ~pure ethanol. In the third column propylene-glycol is the being regenerated.

MOLGROUP



Thank you for your kind attention!